

Selective oxidation of H₂S to elemental sulfur over Ce–V mixed oxide and CeO₂ catalysts prepared by the complexation technique

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Abstract

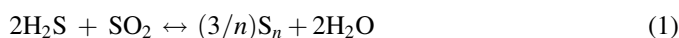
Selective oxidation of H₂S to elemental sulfur was investigated in a fixed bed reactor using Ce–V mixed oxides and cerium oxide (CeO₂) catalytic materials prepared by the complexation technique. The Ce–V mixed oxide with a V/Ce atomic ratio of one and with the CeVO₄ crystal structure gave very high sulfur selectivity values (close to one) at almost complete conversion of H₂S, for O₂/H₂S mole ratios close to 0.5. Best operation temperature was found as 250 °C with this catalyst. CeO₂ gave lower selectivities, causing the formation of some SO₂, even at sub-stoichiometric O₂/H₂S feed ratios. It also showed a fast deactivation due to the partial sulfidation of the catalyst surface during the reaction. XPS analysis of the fresh and the used catalysts containing different V/Ce ratios strongly indicated that the selective oxidation of H₂S to elemental sulfur over the Ce–V mixed oxides involved a redox cycle of cerium, rather than a redox cycle of vanadium.

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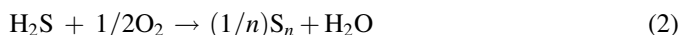
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1. Introduction

In the first step of conventional Claus process for sulfur recovery from process gases, H₂S is partially converted to SO₂ by thermal oxidation at high temperatures and in the second step, unconverted H₂S is reacted with SO₂ in a catalytic converter to produce elemental sulfur. Efficiency of this process is strongly effected by the equilibrium limitations of the second step (Claus reaction).



However, a single step selective oxidation of H₂S to elemental sulfur is practically irreversible and does not have thermodynamic limitations.



Besides the Claus reaction (Eq. (1)), oxidation of the produced sulfur to SO₂ (Eq. (3)) and deep oxidation of H₂S (Eq. (4)) may

cause reduction of sulfur selectivity in the one step selective oxidation of H₂S to elemental sulfur.



Development of active and selective catalysts for this selective oxidation process attracted significant attention of the researchers in recent years [1–7]. In earlier studies, titanium based [8], chromium based [9] and iron based [10] oxide catalysts were proposed for this selective oxidation process. Deactivation of titanium based catalysts in the presence of water vapor, toxic nature of chromium containing materials, and the requirement of excess amount of oxygen for the iron based Superclaus catalyst were reported as some of the drawbacks of these catalysts [2,4,5].

Vanadium based mixed oxide catalysts are known to be highly selective in partial oxidation of hydrocarbons [11,12]. These catalysts also attracted the attention of catalysis researchers working on the selective oxidation of H₂S to elemental sulfur [2–5,13,14]. In the work of Shin et al. [4], which was carried out with V₂O₅ and VO_x/SiO₂ catalysts, and also in our recent study [1], which was carried out with Cu–V and Cu–V–Mo mixed oxide catalysts, it was shown that partially reduced catalysts containing V⁴⁺ were highly selective for the production of elemental sulfur,

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while some amount of SO₂ formation was reported with the oxidized catalysts containing V⁵⁺. A redox reaction mechanism involving the surface lattice oxygen is generally accepted for the selective oxidation of H₂S over these vanadium based mixed oxide catalysts. Deactivation of a vanadium oxide catalyst during the selective oxidation of H₂S was claimed to be due to the slower oxidation rate of the catalyst by the gas phase oxygen as compared to the reduction rate by H₂S [4]. Mixed oxides of vanadium with molybdenum [11], with copper and molybdenum [1], antimony [3,12], titanium, bismuth etc. [5] are reported to show high activity and stability in the selective oxidation reactions, probably due to the improvements in the redox ability of these mixed oxide catalysts. Even in the absence of oxygen gas, formation of some sulfur dioxide and elemental sulfur were reported in our earlier studies [15,16] with the Cu–V and Cu–V–Mo mixed oxides, at temperatures lower than 300 °C. This was concluded to be due to the involvement of surface lattice oxygen of vanadium in the selective oxidation of H₂S. Mixed oxides of vanadium with Mn [19] and Cu [1] were also shown to be very efficient adsorbents for high temperature capture of H₂S.

The redox properties and the high mobility of the capping oxygen of ceria lattice [17] makes it an attractive catalyst for the catalytic oxidation reactions. To improve the selectivity and the catalytic performance in selective partial oxidation reactions, ceria may be modified by the addition of other oxides into its structure [18]. Recently, activities of some rare earth ortovanadates in the selective oxidation of hydrogen sulfide were tested [2] and the activity of cerium ortovanadate was reported to be relatively high.

In the present study, Ce–V mixed oxide catalysts having different V/Ce ratios in their structures and a CeO₂ catalyst were prepared by the complexation technique and the catalytic performances of these materials were investigated for the selective oxidation of H₂S to elemental sulfur.

2. Experimental work

2.1. Catalyst preparation and characterization

In this study, three Ce–V mixed oxide catalysts containing different ratios of V/Ce and a cerium oxide catalytic material containing no vanadium was prepared by the complexation method. In this method, cerium nitrate hexahydrate (Ce(NH₄)₂(NO₃)₆·6H₂O) and ammonium monovanadate were used as the cerium and the vanadium sources, and citric acid was used as the complexation agent, respectively. Equimolar amounts of citric acid and the salts of the metals were mixed in the solution. For the Ce–V mixed oxides, V/Ce ratio was adjusted as 1/3, 2/2 and 3/1, in the three different catalytic materials synthesized. The solution was dehydrated at about 67 °C with continuous stirring, until its viscosity had noticeably increased. Then, this viscous mixture was dried at 75 °C in a glass dish, for 5–11 days. The solid foam was then calcined at 550 °C, for 8 h. Further details of the complexation technique are available in the literature [16].

The catalytic materials synthesized in this work were characterised by BET (Quantachrome), XRD (Philips PW 1840 employing a Cu K α radiation source), SEM, mercury

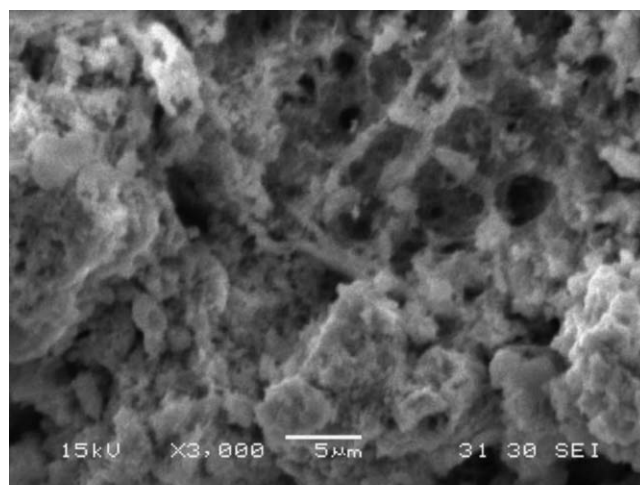
Table 1
Some physical properties of Ce–V mixed oxide catalysts

Catalyst	V/Ce	BET surface area (m ² /g)	Pore volume (cm ³ /g)	Average pore radius (μ m)
CeO ₂	0	50	0.91	0.31
Ce3V1	3/1	47	0.98	0.31
Ce2V2	1	34	0.78	0.43
Ce1V3	1/3	11	0.17	0.13

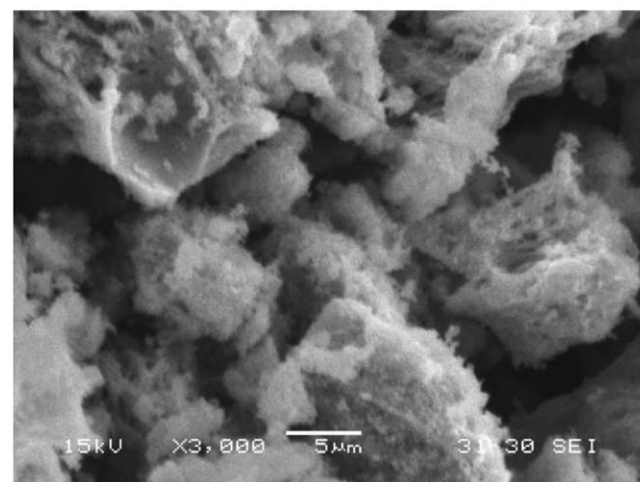
porosimeter (Quantachrome), TPR and XPS (SPECS) measurements. As shown in Table 1, these materials have high porosities and reasonably high surface area values. Higher porosity of the CeO₂ catalyst as compared to a Ce–V mixed oxide catalyst containing equimolar quantities of Ce and V (Ce2V2) is also seen in the SEM photographs (Fig. 1).

2.2. Selective oxidation experiments

H₂S selective oxidation experiments were carried out in a fixed bed quartz reactor packed with 0.2 g of catalyst. An FT-IR Spectrophotometer connected to the exit of the reactor allowed on-line analysis of the reactor exit stream composition.



(a)



(b)

Fig. 1. SEM photographs of (a) CeO₂ and (b) Ce2V2 catalysts.

Concentrations of H₂S, H₂O and SO₂ in the reactor effluent stream were continuously measured. Most of the elemental sulfur was collected in the sulfur condenser placed between the reactor and the FT-IR Spectrophotometer. The temperature of the sulfur condenser was adjusted to 100 °C to allow condensation of the sulfur, while keeping the produced water in the vapor phase. Details of the reaction system and the analysis procedure were reported in our earlier publication [1]. In all these experiments, helium was used as the carrier gas and H₂S concentration was kept as 1%. Total flow rate of the gas mixture was kept constant at 100 cm³/min (measured at 25 °C). Experiments were carried out with O₂/H₂S feed ratios, ranging between 0 and 2.7, in a temperature range of 200–300 °C.

3. Results and discussions

Hydrogen sulfide selective oxidation experiments carried out with the Ce–V mixed oxide catalyst containing a V/Ce atomic ratio of one (Ce2V2) showed the highest elemental sulfur yields at an O₂/H₂S ratio of 0.5. Formation of some SO₂ was observed for O₂/H₂S ratios higher than 0.5, that is higher than the stoichiometric ratio for reaction (2). Some typical results, showing the time dependence of SO₂ and H₂S concentrations measured at the reactor outlet and corresponding to the reactor feed mole fraction ratios of O₂ to H₂S being equal to 0.98 and to zero are given in Fig. 2. This catalyst was found to give highly stable activity in the selective oxidation of H₂S.

Instantaneous fractional conversion of H₂S and the sulfur selectivity were defined as,

$$\text{Fractional conversion} = \frac{(\text{H}_2\text{S})_{\text{in}} - (\text{H}_2\text{S})_{\text{out}}}{(\text{H}_2\text{S})_{\text{in}}}$$

$$S \text{ selectivity} = \frac{(\text{H}_2\text{S})_{\text{in}} - (\text{H}_2\text{S})_{\text{out}} - (\text{SO}_2)_{\text{out}}}{(\text{H}_2\text{S})_{\text{in}} - (\text{H}_2\text{S})_{\text{out}}}$$

The quantitative yields of sulfur were evaluated from the chemical analysis of the reactor exit stream. In our earlier

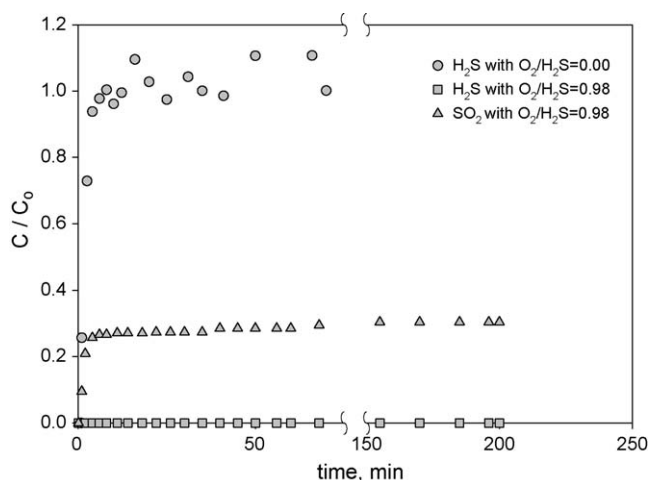


Fig. 2. Fixed bed exit concentrations of H₂S and SO₂ using the Ce2V2 mixed oxide catalyst with O₂/H₂S feed ratios of 0.98 and 0.0, at 250 °C (1% H₂S in the feed stream).

studies, which were conducted for the reaction of H₂S with some mixed metal oxide sorbents in the presence of hydrogen gas [15,16], sulfur balance was also checked by making the chemical analysis of the solid product obtained after the sorption experiments. However, in the present selective oxidation experiments, such a check of sulfur balance could not be made. In these selective oxidation experiments, most of the produced sulfur was collected in the sulfur condenser placed after the reactor. Since the amount of the sulfur produced in our system was too little and the complete collection of the sulfur from the condenser was not possible due to the sticking of some of the sulfur to the walls of the condenser and to the walls of the connecting tubes, precise measurement of the amount of the produced sulfur could not be made. However, the amount of the H₂O produced in our reactor and the amount of the H₂S removed was found to be within the experimental error limits.

In the experiments carried out at 250 °C, 100% conversion of H₂S was obtained for O₂/H₂S feed ratios equal to or higher than 0.5. Some typical values of the steady state conversion and the sulfur selectivity values obtained at different feed compositions are reported in Table 2. For an O₂/H₂S feed ratio of 0.57, a sulfur selectivity value of 0.96 was obtained. Sulfur selectivity decreased with an increase in O₂/H₂S ratio over the stoichiometric value, due to the formation of SO₂.

In an experiment carried out in the absence of oxygen gas, very small amount of H₂S conversion was observed only at the very initial times of the reaction, with the Ce2V2 catalyst. After a few minutes of contact of the reacting gas with the catalyst, no further conversion of H₂S was observed (Fig. 2). This result showed that the catalytic selective oxidation mechanism of the Ce–V mixed oxide was different than the Cu–V mixed oxide investigated in our previous study [1]. For the Cu–V mixed oxide, significant conversion of H₂S to elemental sulfur and the formation of some SO₂ were observed, even in the absence of oxygen gas during the first 50 min of the reaction. This observation had been explained by the involvement of lattice oxygen of Cu–V catalyst in the selective oxidation. In that previous study, it was also shown that V⁵⁺ was reduced to V⁴⁺ and V³⁺ during this process.

The XRD patterns of the Ce2V2 catalyst prepared in the present study showed that, this catalyst was in the CeVO₄ form (Fig. 3a). The XRD patterns of the used catalyst, after the reaction with a stoichiometric feed ratio of O₂/H₂S mixture at 250 °C, indicated no change in the bulk crystal structure (Fig. 3a). However, for the Cu–V mixed oxide catalyst studied in our previous work [1], significant changes were observed in the XRD patterns, after the reaction at similar reaction conditions.

Hydrogen sulfide selective oxidation reactions were repeated at different temperatures in the range between 200

Table 2

Fractional conversion values of H₂S and sulfur selectivities obtained with Ce2V2 catalyst at 250 °C with different O₂/H₂S mole ratios in the feed stream

O ₂ /H ₂ S	0	0.57	0.98	2.70
Fractional conversion of H ₂ S	–	1.0	1.0	1.0
Sulfur selectivity	–	0.96	0.69	0.54

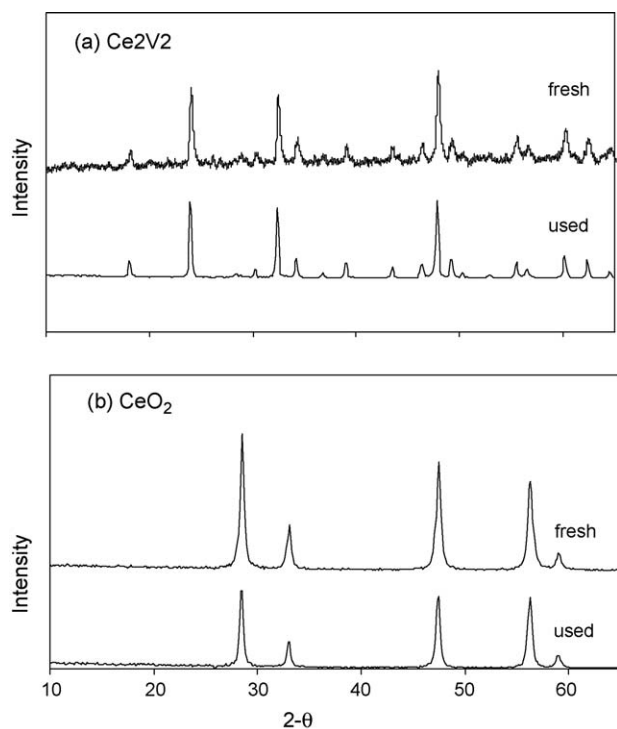


Fig. 3. XRD patterns of the fresh and the used catalysts (after reaction with an O₂/H₂S feed ratio of 0.5 at 250 °C) (a) Ce₂V₂; (b) CeO₂.

and 300 °C, with the Ce₂V₂ mixed oxide catalyst using O₂/H₂S feed ratios close to the stoichiometric value of 0.5. As shown in Fig. 4, the highest H₂S conversion was obtained at 250 °C and the catalyst activity was rather stable at this temperature. Steady state sulfur yields obtained with this catalyst, using a feed mixture containing a O₂/H₂S ratio close to 0.5 (Fig. 5), showed a maximum in the sulfur yield approaching to unity, at around 250 °C. With an increase in temperature, the redox ability of this mixed oxide catalyst is expected to increase. This effect caused an increase in the fractional conversion, in the 200–250 °C temperature range. No SO₂ formation was observed with a stoichiometric feed composition of O₂/H₂S, even at

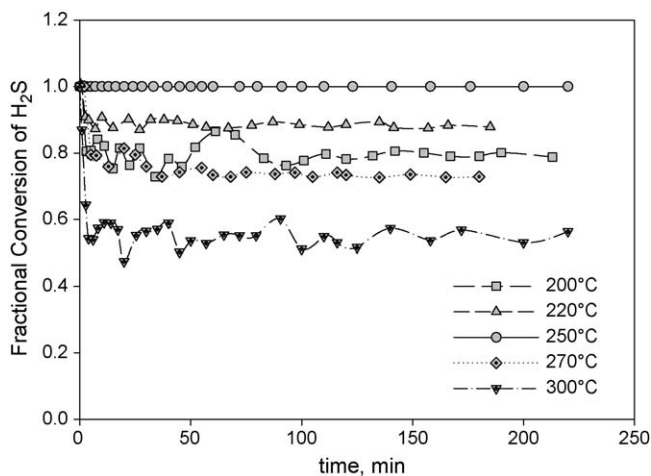


Fig. 4. Fractional conversion of H₂S at different temperatures using the Ce₂V₂ catalyst at near stoichiometric feed compositions.

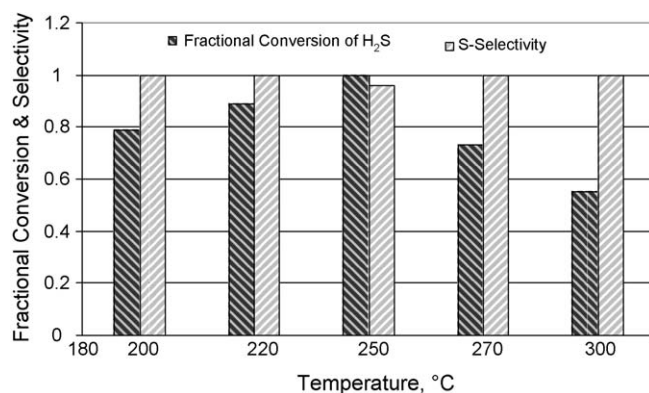


Fig. 5. Variation of the steady state conversion with temperature using the Ce₂V₂ catalyst with a stoichiometric O₂/H₂S feed composition.

temperatures over 250 °C. These results proved the insignificance of reactions (3) and (4) in our system with this Ce–V mixed oxide catalyst, for O₂/H₂S feed ratios close to the stoichiometric value.

The decrease of the steady state fractional conversion of H₂S, with an increase of temperature over 250 °C, may partly be due to the changes in the surface properties of the Ce₂V₂ catalyst at high temperatures. At temperatures over 250 °C, a very sharp decrease of H₂S conversion was observed within the first few minutes of the reaction and then the conversion values became stable (Fig. 4). For instance, at 300 °C, H₂S fractional conversion decreased from 1.0 to about 0.55 within the first few minutes of the reaction and then it became stable at this value. This sharp decrease observed during the first few minutes of the reaction indicated a change in the surface properties of the catalyst at temperatures over 250 °C. In fact, the surface area of the used catalyst after the reaction at 300 °C was found as 19 m²/g, which was about 40% less than the surface area of the fresh catalyst (which was 34 m²/g). In order to further clarify the decrease of the steady state H₂S conversion with an increase in temperature over 250 °C, another set of experiments were carried out with the Ce₂V₂ catalyst, which was pre-treated with a gas stream containing stoichiometric amounts of H₂S and O₂ (O₂/H₂S molar ratio being 0.5) at 500 °C. The steady state H₂S fractional conversion values obtained at different temperatures with this pre-sulfided catalyst (Ce₂V₂–S) are shown in Fig. 6. A maximum was again observed in the H₂S fractional conversion at 250 °C, with this pre-sulfided catalyst. However, this maximum was not as sharp as the corresponding value obtained with the fresh catalyst (Fig. 5). The fractional conversion value obtained at 250 °C with the Ce₂V₂–S catalyst was about 0.63 and it was much less than the fractional conversion value of 1.0, which was obtained with the fresh catalyst at the same temperature. This difference in conversion values indicated an activity decrease of the catalyst after the pre-treatment step with the H₂S containing gas. However, the fractional conversion values of H₂S obtained at 300 °C with the fresh and the pre-sulfided catalysts were found to be quite close to each other, being around 0.55. The decreasing trend of the steady state conversion values obtained with the pre-sulfided catalyst with an increase in temperature over 250 °C (Fig. 6)

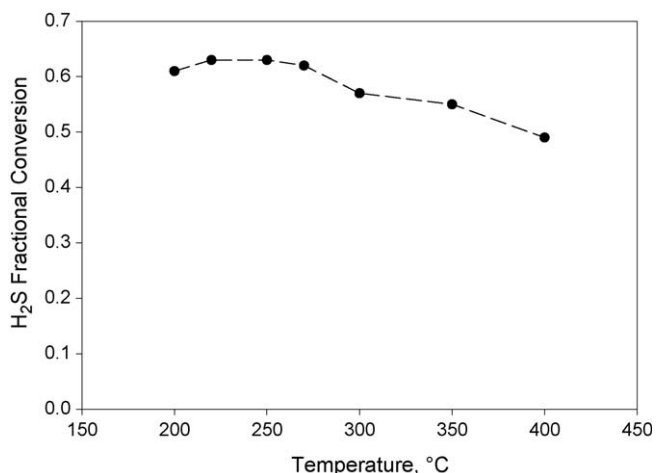


Fig. 6. Temperature dependence of the steady state H₂S conversion using the pre-sulfided catalyst (Ce2V2-S), (O₂/H₂S = 0.5 and 1% H₂S in the feed stream).

may be an indication of a shift in the reaction mechanism at higher temperatures.

The Ce/V ratio of the mixed oxide catalyst is another important parameter for the catalytic performance, in selective oxidation of H₂S. The activities of the three mixed oxide catalysts containing Ce/V ratios of 3/1, 2/2 and 1/3 were rather stable throughout the selective oxidation experiments lasting about 4 h. However, a significant decrease of the activity of pure cerium oxide catalyst was observed during the reaction. For the pure CeO₂ catalyst, the decrease of H₂S fractional conversion with reaction time is illustrated in Fig. 7, at 250 and 300 °C reaction temperatures. A rather sharp decrease of the activity of this catalyst was observed, especially after about 100 min of contact. It was interesting to see that the XRD patterns of the fresh and the used cerium oxide catalysts were similar, indicating that the bulk of this catalyst was in cerianite (CeO₂) structure (Fig. 3b), before and after the reaction. Deactivation of the CeO₂ catalyst during the course of the reaction, without a significant change in its bulk structure, is

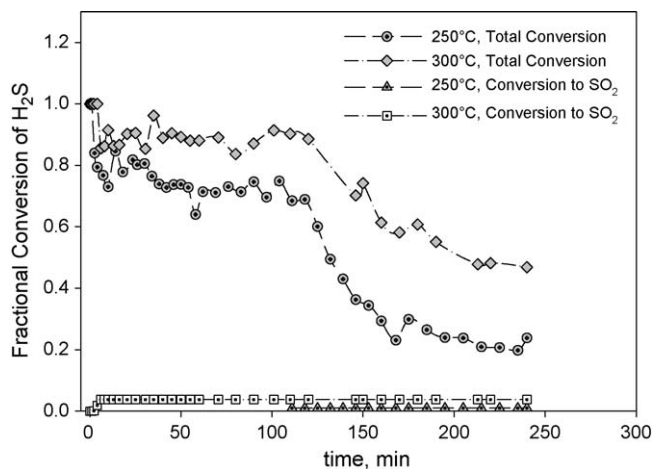


Fig. 7. Activity variation of the CeO₂ catalyst during reaction with an O₂/H₂S feed ratio of 0.5 at different temperatures.

probably due to the faster depletion rate of the capping oxygen layer on the catalyst surface than the reoxidation rate by gaseous oxygen and the resulting changes in the surface structure of the catalyst.

The XPS analysis of the fresh and the used CeO₂ catalysts justified the changes on surface properties of this catalyst (Fig. 8a) after the reaction. The characteristic sulfur signal (S 2p₃) observed at 166.2 eV clearly showed the formation of a sulfided layer over the CeO₂ catalyst during the selective oxidation reaction of H₂S. Also, the difference in the 3d_{5/2} signals of cerium in the fresh and the used CeO₂ catalysts indicated the partial reduction of the oxidation state of surface Ce atoms from +4 to +3, after the sulfidation reaction. The intensity of the characteristic 3d_{5/2} signal of Ce⁴⁺ at 882.2 eV decreased and the intensity of the signal at 885.8 eV increased, after the sulfidation reaction (Fig. 8a). Quantitative analysis of the XPS results indicated a S/Ce atomic ratio of about 0.8, on the surface of the used CeO₂ catalyst. These changes indicated the formation of cerium sulfates on the surface, which was

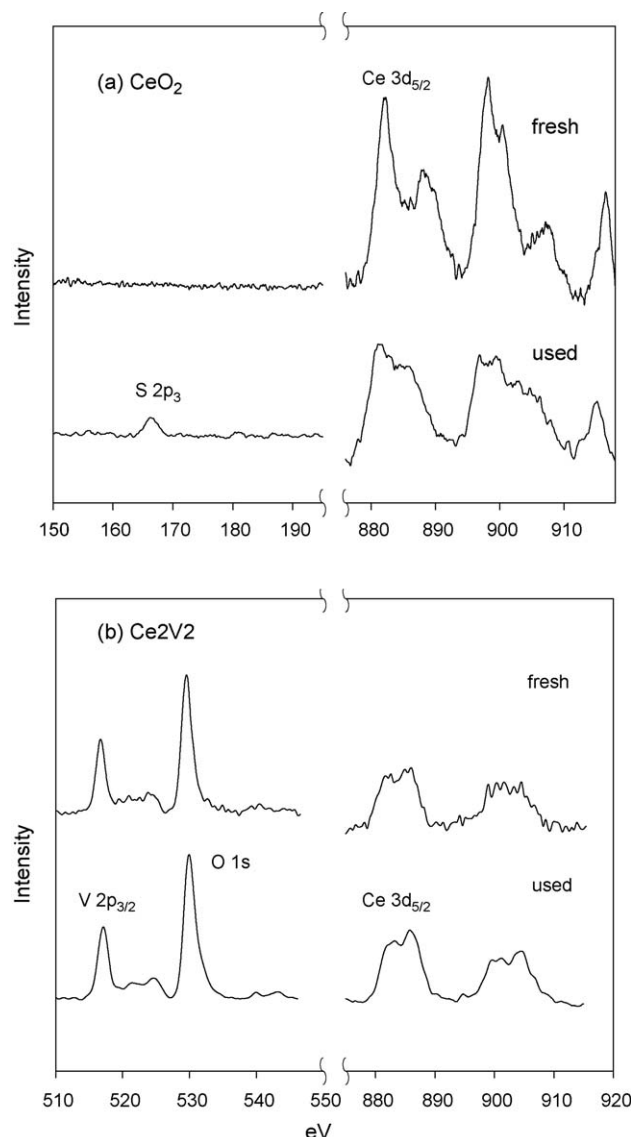


Fig. 8. XPS analysis of the fresh and the used catalysts (a) CeO₂ (b) Ce2V2.

thought to cause the deactivation of this catalyst. In the thermodynamic analysis reported by Ferrizz et al. [22], Ce–O–S phase diagrams, sulfide and sulfate formation under reducing and oxidizing conditions are discussed.

Another interesting observation was that the activity of CeO₂ catalyst was higher at 300 °C than the corresponding values at 250 °C (Fig. 7). However, for the Ce2V2 mixed oxide catalyst the maximum activity was observed at 250 °C. At 250 °C, the fractional conversion of H₂S was about unity with the Ce2V2 catalyst, while the corresponding fractional conversion obtained with the CeO₂ catalyst (at times smaller than 100 min) was less than 0.8. Temperature programmed reduction (TPR) profiles of the CeO₂ and the Ce2V2 catalysts (Fig. 9) suggested some explanation for this observation. TPR profiles of both of these catalysts showed two broad peaks. The maximum of the first TPR peak appeared at about 550 °C and this was considered to be due to the reduction of the surface capping oxygen of ceria. A similar result was reported by Zhu et al. [20] in a study for CO oxidation over a Pd/CeO₂ catalyst. The interesting observation of hydrogen TPR of these two catalysts was that, the reduction of the Ce2V2 catalyst started at about 250 °C, while the reduction of CeO₂ started at a higher temperature (over 350 °C). These results indicated an improvement of the redox ability of the ceria catalyst at lower temperatures by the incorporation of vanadia into the catalyst structure. The second TPR peak observed at 780 °C for the

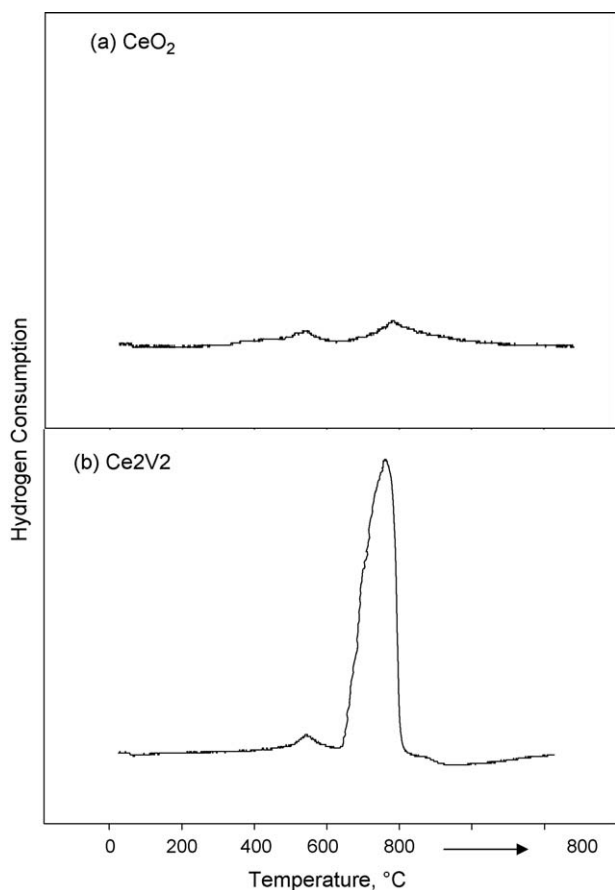


Fig. 9. Hydrogen TPR profiles of CeO₂ and Ce2V2 catalysts.

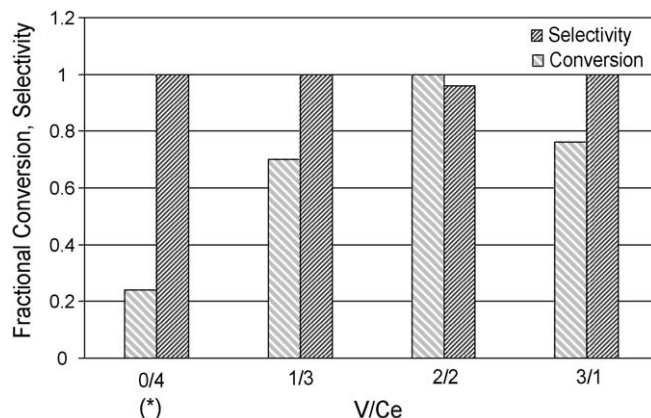


Fig. 10. H₂S fractional conversion and sulfur selectivity values obtained at 250 °C with the catalysts having different V/Ce ratios (O₂/H₂S = 0.5). [(*) At a reaction time of 200 min].

CeO₂ catalyst corresponds to the reduction of the bulk lattice oxygen. For the Ce2V2 catalyst, the second broad peak was observed at 763 °C and it was much bigger than the corresponding TPR peak observed with pure CeO₂. This broad peak obtained at 763 °C corresponds to the removal of oxygen from the bulk of CeVO₄, resulting the reduction of V⁺⁵.

The steady state conversion and the sulfur selectivity values obtained at 250 °C with the Ce–V mixed oxide catalysts having different Ce/V ratios and using a feed stream containing stoichiometric ratio of O₂/H₂S are shown in Fig. 10. In the same figure, conversion and sulfur selectivity values obtained with the CeO₂ catalyst, at a reaction time of 200 min, are also given. For all these cases, sulfur selectivities were about unity. However, the highest conversion of H₂S was observed with the catalyst containing equal moles of cerium and vanadium (Ce2V2). The BET surface area and the pore volume of the catalyst containing a V/Ce mole ratio of three is much lower than the other catalysts containing lower V/Ce ratios. This is one of the factors causing the lower activity of this catalyst. More importantly, crystal structures and the oxidation states of V and Ce in the Ce–V mixed oxide catalysts determine the activity of these catalysts.

The XRD patterns of all these catalysts are given in Fig. 11. These XRD patterns showed the presence of both CeVO₄ and CeO₂ phases in the Ce3V1 catalyst, while the Ce2V2 catalyst contained only CeVO₄ phase. The Ce1V3 catalyst was more amorphous and the presence of some CeVO₄ phase was also

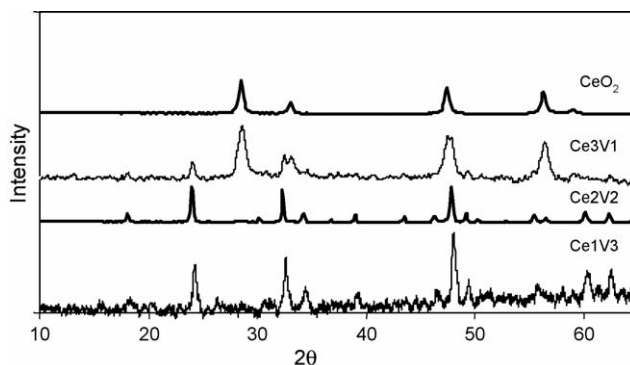


Fig. 11. XRD patterns of the catalysts with different V/Ce ratios.

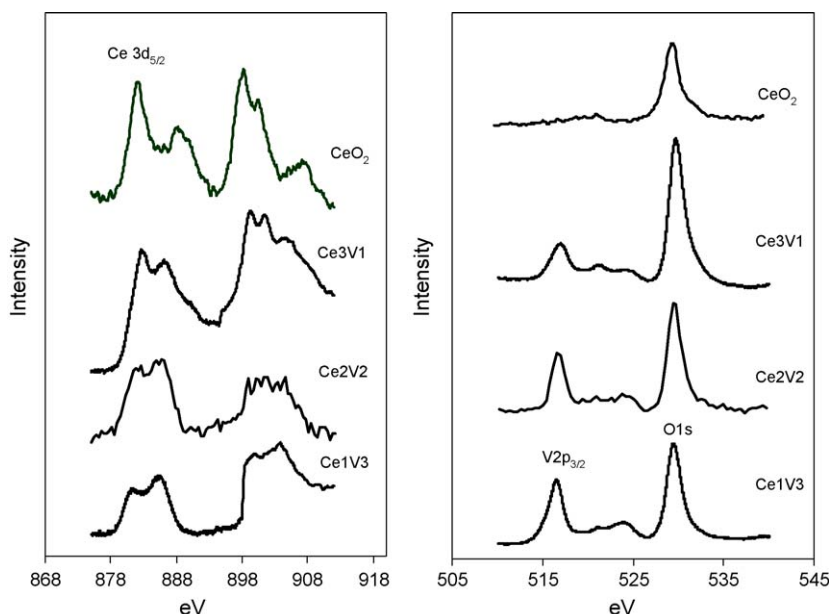


Fig. 12. XPS analysis of the catalysts with different V/Ce ratios.

observed. The XPS analysis of these mixed oxide catalysts showed that vanadium was in the oxidation state of +5, in all of them (Fig. 12 and Table 3). $V2p_{3/2}$ binding energies of all these catalysts were between 517.1 and 517.2 eV and the difference in binding energies between O1s and $V2p_{3/2}$ (Δ_{O-V}) were about 12.7–12.6 eV, indicating +5 oxidation state of vanadium. The details of XPS binding energies of different vanadium oxidation states are reported by Silversmit et al. [21]. Comparison of the XPS analysis of the fresh and the used Ce2V2 catalysts also indicated that oxidation state of vanadium did not change after the selective oxidation reaction (Fig. 8b). The $V2p_{3/2}$ signal observed at 517.1 eV in the XPS analysis of the fresh and the used Ce2V2 catalyst justified this. In contrary to the CeO₂ catalyst, the XPS analysis of the Ce2V2 catalyst showed that there was no sulfur on the catalyst surface after the sulfidation reaction. No XPS signal was observed at around 166.2 eV for the fresh and the used Ce2V2 catalysts. As reported above, this catalyst was rather stable and showed no deactivation throughout the selective oxidation reaction at 250 °C.

As shown in Fig. 12 and as summarized in Table 3, the binding energy of Ce3d_{5/2} at 882.2 eV indicated that most of the cerium was in +4 oxidation state in the CeO₂ catalyst. In the case of mixed oxide catalysts, formation of CeVO₄ structure was observed. In this phase, cerium was in +3 oxidation state. The two peaks observed at about 881.8 and 885.8 eV for the Ce3d_{5/2} indicated the presence of +4 and +3 oxidation states of

cerium in the mixed oxide catalysts. For the most active mixed oxide catalyst containing equal amounts of cerium and vanadium (Ce2V2), most of the cerium was in +3 oxidation state. For the catalyst containing higher amount of cerium (Ce3V1), most of the cerium was in +4 oxidation state. Results showed that V enhanced the stability of the +3 oxidation state of cerium in the catalyst structure.

The XPS results of the fresh and the used mixed oxide catalysts containing equal amounts of V and Ce (Ce2V2) showed some increase in the ratio of signals observed at 885.3 and 881.8 eV, after the sulfidation reaction (Fig. 8b). This increase indicated further reduction of the surface Ce atoms from +4 to +3 state during the sulfidation reaction. However, no change in the oxidation state of V (+5) was observed after the reaction. All these results showed that for the Ce2V2 catalyst containing CeVO₄, vanadium and cerium were majorly in V⁵⁺ and Ce³⁺ oxidation states and the selective oxidation of H₂S to elemental sulfur most probably involved a redox cycle of cerium, rather than a redox cycle of vanadium. This conclusion is in agreement with the conclusion of Martinez-Huerta et al. [18] who studied the nature of vanadia-ceria interface in V⁵⁺/CeO₂ catalysts.

4. Concluding remarks

A Ce–V mixed oxide catalyst containing equimolar quantities of cerium and vanadium gave very high sulfur yields approaching to unity, in the selective oxidation of H₂S with a feed stream containing equimolar quantities of oxygen and H₂S. Incorporation of vanadium into the ceria structure improved the redox ability of ceria at low temperatures and stabilized its activity in the H₂S selective oxidation. However, the activity of pure CeO₂ was found to show a decrease during the reaction due to the formation of a partially sulfided layer on the catalyst surface. The active phase of the mixed oxide was found as CeVO₄ and this catalyst showed the highest activity at 250 °C.

Table 3
XPS Analysis of Ce–V oxide catalysts prepared in this work

Sample	O1s (eV)	V2p _{3/2} (eV)	$\Delta_{(O-V)}$ (eV)	Ce3d _{5/2} (eV)
CeO ₂	529.6	–	–	882.2
Ce3V1	529.8	517.1	12.7	882.5
Ce2V2	529.8	517.1	12.7	885.3–881.8
Ce1V3	529.8	517.2	12.6	885.2–881.6

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